

# **Field-based Parameterisation of Cardiac Muscle Structure from Diffusion Tensors**

Diffusion tensor calculation

equation proposed by Basser et al.<sup>1</sup>

Bianca Freytag, Vicky Wang, Richard Christie, Alexander Wilson, Gregory Sands, Ian LeGrice, Alistair Young, Martyn Nash

## Background

Diffusion tensor MRI exploits Brownian motion of water molecules within soft tissue (e.g. brain, heart) to determine local anisotropic diffusion<sup>1</sup>. The direction of maximum water diffusion, represented by the primary eigenvector of the derived diffusion tensor, has been found to correlate well with the local histologically-measured myofibre orientation<sup>2,3</sup>

Fibre orientations of the heart, derived from diffusion tensors, are often represented as fibre angles with respect to the short-axis plane of the heart.

There are two main disadvantages in using the primary eigenvector to calculate fibre orientations:

i. Water diffuses equally in opposite directions but the primary eigenvector arbitrarily represents just one of these directions (see Fig. 1).



ii. In regions of apparent near-isotropic diffusion, indicated by a low fractional anisotropy (FA), the eigenvector may not reliably represent the local tissue microstructure (see Fig. 2).



## **Motivation**

We present a workflow for model-based parameterisation of myocardial fibre fields directly from the diffusion tensors to circumvent the above disadvantages.

## Method



#### Image segmentation

Endocardial and epicardial surfaces of the LV were manually segmented from the non-diffusion images using MATLAB.

The contours were transformed to the cardiac coordinate system defined by three landmark points (centroids of the LV base, LV apex, and RV base) selected from the non-diffusion weighted image.



Fig. 5: Fitted FE LV model

### Field-based parameterisation of LV fibre orientation

The FE fibre angle field was initialised by setting the fibre angles to  $\theta_n = +60^\circ$  (endocardial nodes), and  $\theta_n = -70^\circ$ (epicardial nodes). Imbrication angles ( $\varphi_n$ ) of all nodes were set to be 0°. These angles were interpolated over the FE model with tricubic-Hermite basis functions.

For each voxel (v) the FE local coordinates within the LV geometric model were determined. At those locations the myofibre orientation  $f_{n_i}$  defined by Euler angle rotations (using interpolated  $\theta$  and  $\varphi$ ), was computed.

An objective function was constructed to maximise the local diffusion direction  $f_{\nu}$  by modifying the nodal fibre parameters ( $\theta_v$  and  $\varphi_v$ ).





**Results** 

variation as expected (see Fig. 7).



The fitted fibre angle field showed a smooth transmural

In regions with high FA values, the fitted fibre orientations correlated well with the primary eigenvectors as indicated by the dot product map shown in Fig. 8 (a). This correlation was low in regions with low FA as highlighted in Fig. 8 (b).



## Conclusion

This novel method to construct a model-based myocardial fibre field does not need to compute eigenvectors or FA values and circumvents issues associated with phaseunwrapping of eigenvectors prior to fibre fitting. It also helps to ensure that the interpolated fibre angles in regions with high FA are better representations of the diffusion tensors.

The workflow could be adapted to construct fibre fields using in vivo cardiac imaging data and associated geometric FE models for individualised analyses of heart mechanics.

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Fig. 4: Segmented surfaces and landmark points



## LV FE geometric model construction

estimated for each voxel by solving the logarithm of the diffusion

 $\log(S_k) = \log(S_0) - b \sum_{i=1}^{3} \sum_{j=1}^{3} (\boldsymbol{Q}_k)_{ij} D_{ij}$ 

A 16-element tricubic-Hermite FE model was customised to the surface contours obtained from Step 2. The endocardial and epicardial surfaces of the model were fitted to best match the corresponding surface data.



 $F = \sum_{\nu=1}^{N} (f_{\nu}')$  where  $f_{\nu}' = f_{i,\nu} D_{i,\nu} f_{i,\nu}$ 

summed over *i*. *i* 

v = 1. N is the number of voxels